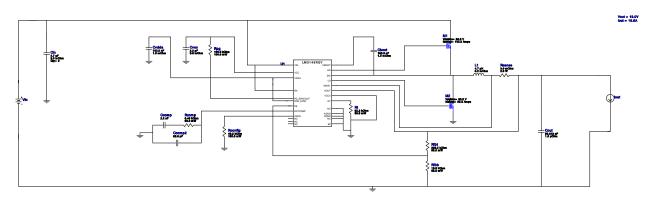


VinMin = 24.0V VinMax = 24.0V Vout = 19.0V lout = 15.5A Device = LM5148RGYR Topology = Buck Created = 2025-02-24 10:48:52.182 BOM Cost = NA BOM Count = 19 Total Pd = 4.08W

# WEBENCH® Design Report

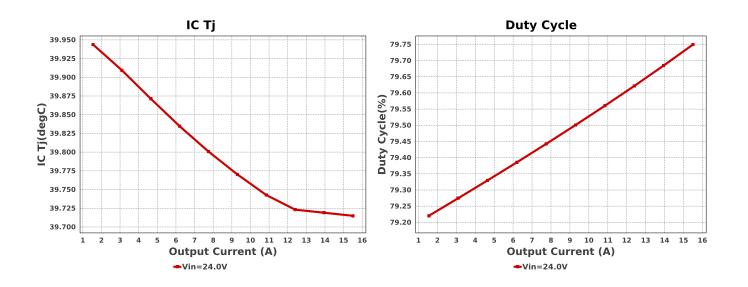
Design: 46 LM5148RGYR LM5148RGYR 24V-24V to 19.00V @ 15.5A

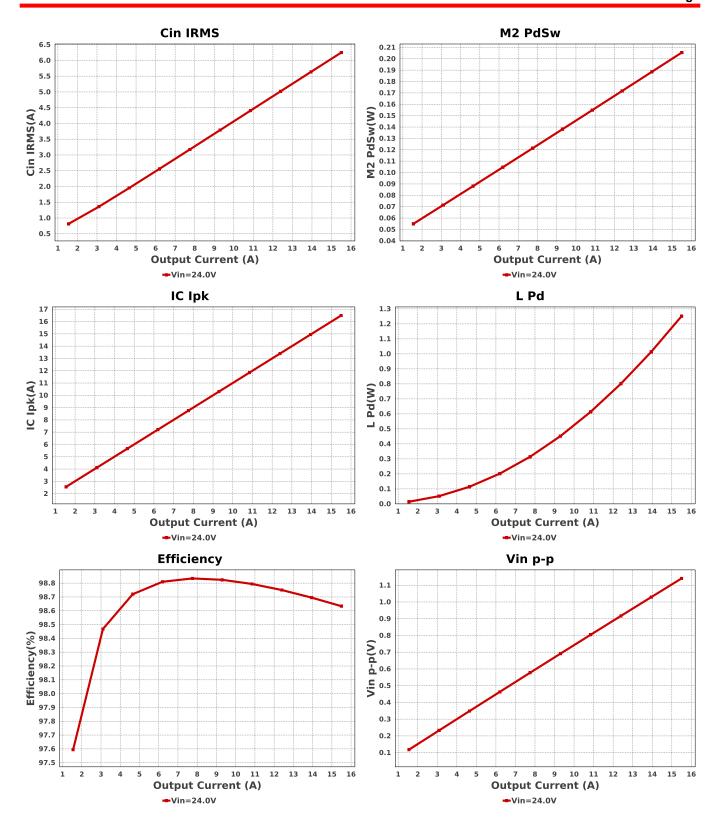


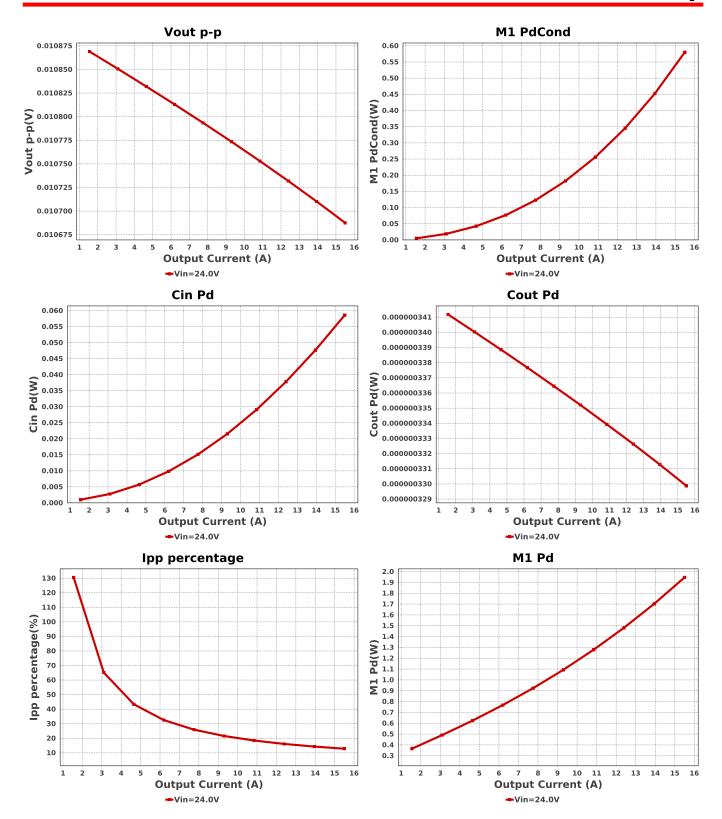
#### **Electrical BOM**

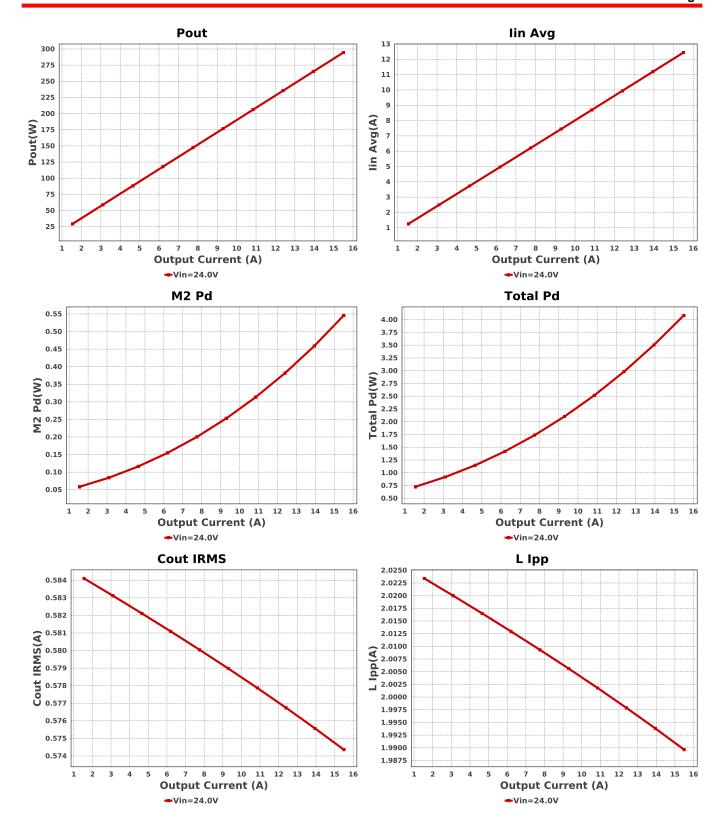
Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Cboot	MuRata	GRM155R71A104KA01D Series= X7R	Cap= 100.0 nF ESR= 1.0 mOhm VDC= 10.0 V IRMS= 0.0 A	1	\$0.01	0402 3 mm <sup>2</sup>
Ccomp	Samsung Electro- Mechanics	CL21C222JBFNNNE Series= C0G/NP0	Cap= 2.2 nF VDC= 50.0 V IRMS= 0.0 A	1	\$0.02	0805 7 mm <sup>2</sup>
Ccomp2	Yageo	CC0805JRNPO9BN820 Series= C0G/NP0	Cap= 82.0 pF VDC= 50.0 V IRMS= 0.0 A	1	\$0.01	0805 7 mm <sup>2</sup>
Cin	MuRata	GRM31CR71H475KA12L Series= X7R	Cap= 4.7 uF ESR= 3.0 mOhm VDC= 50.0 V IRMS= 4.98 A	2	\$0.10	1206 11 mm <sup>2</sup>
Cout	CUSTOM	CUSTOM Series= ?	Cap= 56.342 uF ESR= 1.0 uOhm VDC= 28.5 V IRMS= 631.85 mA	1	NA	CUSTOM 0 mm <sup>2</sup>
Cvcc	MuRata	GRM188R71A225KE15D Series= X7R	Cap= 2.2 uF ESR= 9.0 mOhm VDC= 10.0 V IRMS= 3.3 A	1	\$0.02	0603 5 mm <sup>2</sup>
Cvdda	MuRata	GRM155R71A104KA01D Series= X7R	Cap= 100.0 nF ESR= 1.0 mOhm VDC= 10.0 V IRMS= 0.0 A	1	\$0.01	0402 3 mm <sup>2</sup>
L1	Coilcraft	XAL1010-472MEB	L= 4.7 μH 5.2 mOhm	1	\$1.71	
						XAL1010 160 mm <sup>2</sup>
M1	Texas Instruments	CSD17303Q5	VdsMax= 30.0 V IdsMax= 100.0 Amps	1	\$0.56	TRANS_NexFET_Q5 55 mm²

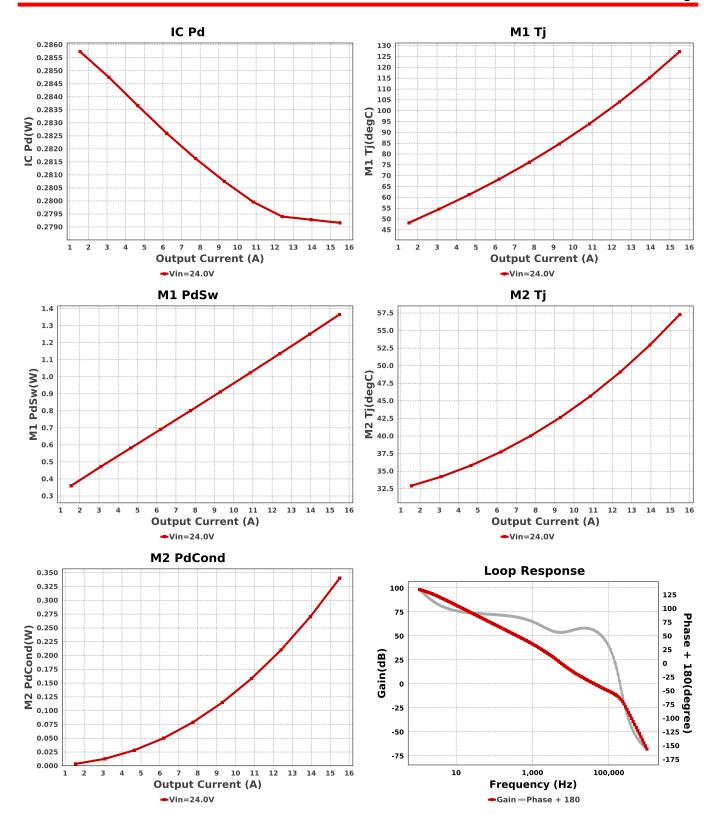
Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
M2	Texas Instruments	CSD17577Q5A	VdsMax= 30.0 V ldsMax= 60.0 Amps	1	\$0.17	TRANS_NexFET_Q5A 55 mm²
Rcomp	Vishay-Dale	CRCW04028K45FKED Series= CRCWe3	Res= 8.45 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm <sup>2</sup>
Rconfig	Vishay-Dale	CRCW060340K2FKEA Series= CRCWe3	Res= 40.2 kOhm Power= 100.0 mW Tolerance= 1.0%	1	\$0.01	0603 5 mm <sup>2</sup>
Rfbb	Vishay-Dale	CRCW040210K0FKED Series= CRCWe3	Res= 10.0 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm <sup>2</sup>
Rfbt	Vishay-Dale	CRCW0402226KFKED Series= CRCWe3	Res= 226.0 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm <sup>2</sup>
Rpg	Vishay-Dale	CRCW0603100KFKEA Series= CRCWe3	Res= 100.0 kOhm Power= 100.0 mW Tolerance= 1.0%	1	\$0.01	0603 5 mm <sup>2</sup>
Rsense	Vishay-Dale	WSR23L000FEA Series= WSR	Res= 3.0 mOhm Power= 2.0 W Tolerance= 1.0%	1	\$0.74	4527 122 mm <sup>2</sup>
Rt	Vishay-Dale	CRCW040252K3FKED Series= CRCWe3	Res= 52.3 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm <sup>2</sup>
U1	Texas Instruments	LM5148RGYR	Switcher	1	\$0.60	RGY0024F 43 mm²

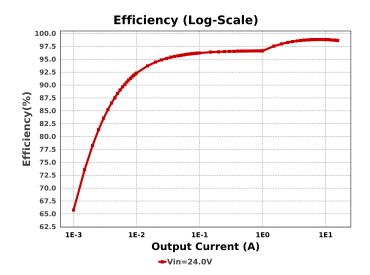












## **Operating Values**

#	Name	Value	Category	Description
1.	BOM Count	19		Total Design BOM count
2.	Total BOM	NA		Total BOM Cost
3.	Cin IRMS	6.25 A	Capacitor	Input capacitor RMS ripple current
4.	Cin Pd	58.594 mW	Capacitor	Input capacitor power dissipation
5.	Cout IRMS	574.356 mA	Capacitor	Output capacitor RMS ripple current
6.	Cout Pd	329.88 nW	Capacitor	Output capacitor power dissipation
7.	IC lpk	16.495 A	IC	Peak switch current in IC
8.	IC Pd	279.16 mW	IC	IC power dissipation
9.	IC Tj	39.715 degC	IC	IC junction temperature
10.	IC Tolerance	10.0 mV	IC	IC Feedback Tolerance
11.	ICThetaJA Effective	34.8 degC/W	IC	Effective IC Junction-to-Ambient Thermal Resistance
12.	lin Avg	12.441 Å	IC	Average input current
13.	lpp percentage	12.836 %	Inductor	Inductor ripple current percentage (with respect to average inductor
	.pp porocinago	.2.000 /0		current)
14.	L lpp	1.99 A	Inductor	Peak-to-peak inductor ripple current
	L Pd	1.251 W	Inductor	Inductor power dissipation
	M1 Pd	1.946 W	Mosfet	M1 MOSFET total power dissipation
_	M1 PdCond	580.02 mW	Mosfet	M1 MOSFET conduction losses
18.	M1 PdSw	1.366 W	Mosfet	M1 MOSFET switching losses
	M1 Tj	127.302 degC	Mosfet	M1 MOSFET junction temperature
	M2 Pd	545.67 mW	Mosfet	M2 MOSFET total power dissipation
	M2 PdCond	340.22 mW	Mosfet	M2 MOSFET conduction losses
	M2 PdSw	205.46 mW	Mosfet	M2 MOSFET switching losses
	M2 Tj	57.284 degC	Mosfet	M2 MOSFET junction temperature
	Cin Pd	58.594 mW	Power	Input capacitor power dissipation
	Cout Pd	329.88 nW	Power	Output capacitor power dissipation
26.	IC Pd	279.16 mW	Power	IC power dissipation
	L Pd	1.251 W	Power	Inductor power dissipation
28.	M1 Pd	1.946 W	Power	M1 MOSFET total power dissipation
29.	M1 PdCond	580.02 mW	Power	M1 MOSFET conduction losses
30.	M1 PdSw	1.366 W	Power	M1 MOSFET switching losses
	M2 Pd	545.67 mW	Power	M2 MOSFET total power dissipation
32.	M2 PdCond	340.22 mW	Power	M2 MOSFET conduction losses
33.	M2 PdSw	205.46 mW	Power	M2 MOSFET switching losses
34.	Total Pd	4.082 W	Power	Total Power Dissipation
35.	Cross Freq	39.907 kHz	System	Bode plot crossover frequency
			Information	
36.	Duty Cycle	79.75 %	System	Duty cycle
			Information	
37.	Efficiency	98.633 %	System	Steady state efficiency
	,		Information	, , , , , , , , , , , , , , , , , , , ,
38.	FootPrint	602.0 mm <sup>2</sup>	System	Total Foot Print Area of BOM components
	- =	502.0 mm	Information	
39.	Frequency	415.541 kHz	System	Switching frequency
55.	1 Toquotioy	110.0+1 KHZ	Information	Sintorning inequation
40.	Gain Marg	-11.663 dB	System	Bode Plot Gain Margin
<del>4</del> 0.	Gairi iviary	-11.003 UD	•	Boue Flot Galli Margin
11	lout	15 5 A	Information	lout aparating point
41.	lout	15.5 A	System	lout operating point
46		17.75.4	Information	
42.	lout transient step use	ed 7.75 A	System	Custom Transient current step requirement that was used for Cout
	for Cout calculations		Information	selection (A).

#	Name	Value	Cotogory	Description
			Category	Description Coin at 411-
43.	Low Freq Gain	97.827 dB	System	Gain at 1Hz
4.4	Marila	0014	Information	Open destina Maria
44.	Mode	CCM	System	Conduction Mode
45	O complete to the last	400.057\/	Information	The area Caral March Occasion and Malaca
45.	Overshoot Value	132.657 mV	System	Theoretical Vout Overshoot Value
40	D	00.004	Information	
46.	Phase Marg	60.981 deg	System	Bode Plot Phase Margin
			Information	
47.	Pout	294.5 W	System	Total output power
			Information	
48.	Undershoot Value	573.48 mV	System	Theoretical Vout Undershoot Value
			Information	
49.	Vin	24.0 V	System	Vin operating point
			Information	
50.	Vin p-p	1.141 V	System	Peak-to-peak input voltage
			Information	
51.	Vout	19.0 V	System	Operational Output Voltage
			Information	
52.	Vout Actual	18.88 V	System	Vout Actual calculated based on selected voltage divider resistors
			Information	
53.	Vout Ripple	1.0 %	System	Custom maximum output ripple requirement that was used for Cout
	requirement used for		Information	selection(% of Vout).
	Cout calculations			
54.	Vout Tolerance	3.209 %	System	Vout Tolerance based on IC Tolerance (no load) and voltage divider
			Information	resistors if applicable
55.	Vout p-p	10.688 mV	System	Peak-to-peak output ripple voltage
			Information	
56.	Vout transient	3.0 %	System	Custom Transient voltage change requirement that was used for Cout
	requirement used for		Information	selection (% of Vout).
	Cout calculations			

### **Design Inputs**

3 1			
Name	Value	Description	
lout	15.5	Maximum Output Current	
VinMax	24.0	Maximum input voltage	
VinMin	24.0	Minimum input voltage	
Vout	19.0	Output Voltage	
base_pn	LM5148	Base Product Number	
source	DC	Input Source Type	
Та	30.0	Ambient temperature	

### WEBENCH® Assembly

#### Component Testing

Some published data on components in datasheets such as Capacitor ESR and Inductor DC resistance is based on conservative values that will guarantee that the components always exceed the specification. For design purposes it is usually better to work with typical values. Since this data is not always available it is a good practice to measure the Capacitance and ESR values of Cin and Cout, and the inductance and DC resistance of L1 before assembly of the board. Any large discrepancies in values should be electrically simulated in WEBENCH to check for instabilities and thermally simulated in WebTHERM to make sure critical temperatures are not exceeded.

#### Soldering Component to Board

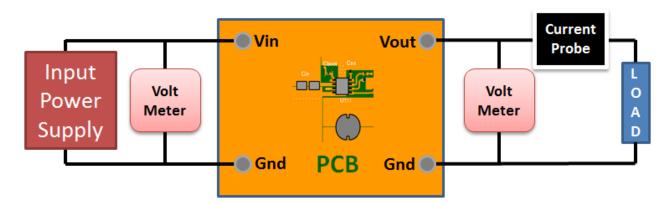
If board assembly is done in house it is best to tack down one terminal of a component on the board then solder the other terminal. For surface mount parts with large tabs, such as the DPAK, the tab on the back of the package should be pre-tinned with solder, then tacked into place by one of the pins. To solder the tab town to the board place the iron down on the board while resting against the tab, heating both surfaces simultaneously. Apply light pressure to the top of the plastic case until the solder flows around the part and the part is flush with the PCB. If the solder is not flowing around the board you may need a higher wattage iron (generally 25W to 30W is enough).

#### Initial Startup of Circuit

It is best to initially power up the board by setting the input supply voltage to the lowest operating input voltage 24.0V and set the input supply's current limit to zero. With the input supply off connect up the input supply to Vin and GND. Connect a digital volt meter and a load if needed to set the minimum lout of the design from Vout and GND. Turn on the input supply and slowly turn up the current limit on the input supply. If the voltage starts to rise on the input supply continue increasing the input supply current limit while watching the output voltage. If the current increases on the input supply, but the voltage remains near zero, then there may be a short or a component misplaced on the board. Power down the board and visually inspect for solder bridges and recheck the diode and capacitor polarities. Once the power supply circuit is operational then more extensive testing may include full load testing, transient load and line tests to compare with simulation results.

#### Load Testing

The setup is the same as the initial startup, except that an additional digital voltmeter is connected between Vin and GND, a load is connected between Vout and GND and a current meter is connected in series between Vout and the load. The load must be able to handle at least rated output power + 50% (7.5 watts for this design). Ideally the load is supplied in the form of a variable load test unit. It can also be done in the form of suitably large power resistors. When using an oscilloscope to measure waveforms on the prototype board, the ground leads of the oscilloscope probes should be as short as possible and the area of the loop formed by the ground lead should be kept to a minimum. This will help reduce ground lead inductance and eliminate EMI noise that is not actually present in the circuit.



#### **Design Assistance**

- 1. Master key: F99F3073C415E694101A56F6FF7B20CC[v1]
- 2. LM5148 Product Folder: http://www.ti.com/product/LM5148: contains the data sheet and other resources.

#### Important Notice and Disclaimer

TI provides technical and reliability data (including datasheets), design resources (including reference designs), application or other design advice, web tools, safety information, and other resources AS IS and with all faults, and disclaims all warranties. These resources are intended for skilled developers designing with TI products. You are solely responsible for (1) selecting the appropriate TI products for your application, (2) designing, validating and testing your application, and (3) ensuring your application meets applicable standards, and any other safety, security, or other requirements.

These resources are subject to change without notice. TI grants you permission to use these resources only for development of an application that uses the TI products described in the resource. Other reproduction and display of these resources is prohibited. No license is granted to any other TI intellectual property right or to any third party intellectual property right. TI disclaims responsibility for, and you will fully indemnify TI and its representatives against, any claims, damages, costs, losses, and liabilities arising out of your use of these resources.

Providing these resources does not expand or otherwise alter TI's applicable Terms of Sale or other applicable terms available either on ti.com or provided in conjunction with TI products.